INTRODUCTION

The purpose of these Guidelines is to provide insight into the basic stability concepts relevant to loading and to loaded pontoon barges.

Pontoon barges are used for a wide variety of cargoes from bulk loads such as coal, rock, and logs – with low to medium centres of gravity – through to vehicles, and unique “one-off” loads such as industrial equipment and storage tanks, which can have very high centres of gravity, and windage areas. Pontoon barges are also used as work platforms for many types of equipment including cranes and pile drivers.

Stability considerations are critical when conducting transportation and other marine operations safely.

The guidance that follows only deals with stability. It is assumed that other aspects of best marine practice – such as having sufficient handling power (bollard pull), and manoeuvring capability, watertightness arrangements (including securing of hatches etc), and ensuring adequacy of tow rigging, emergency, and safety gear – have also all been addressed.
Understanding and managing the stability of your barge is critical to the safety of you and your crew, and to the safe delivery of your cargo. The following basic rules offer step by step guidance aimed at ensuring safety and success. In case of any doubt appropriate advice must be obtained prior to agreeing to undertake a marine operation. Differences in cargoes, environment, routing, equipment and crewing make each situation unique.

Proper planning is common sense – safety is no accident.

1. Know the lightship displacement of the barge before loading.
2. Know the lightship centre of gravity (KG) for the barge.
3. Know the weight and centre of gravity of the cargo.
4. Be aware of the block coefficient of the barge.
5. Be aware of initial metacentric height (GM) and know how to calculate it for the loaded barge using the rectangular block formula.
6. Know how to calculate the combined KG for the barge loaded with its cargo.
7. Be aware of the limiting KG curve, and have one available for guidance in loading your barge.
8. Talk to a Maritime NZ recognised Ship Surveyor about conducting an inclining experiment and make contact with a Maritime NZ recognised Naval Architect to obtain a limiting KG curve for your barge.
9. Always check the loading and discharge conditions as well as the loaded cargo condition for the barge.
10. Take special care that cargo is properly secured, and that free surface effects are minimised, when using cranes or other equipment that may affect the stability of the barge.

Consult a Maritime NZ recognised Ship Surveyor, or Naval Architect in any cases of doubt.
**ILLUSTRATION ONE** – **STABLE / UNSTABLE VESSEL**

**ILLUSTRATION ONE GLOSSARY**

<p>| | |</p>
<table>
<thead>
<tr>
<th></th>
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</thead>
<tbody>
<tr>
<td>K</td>
<td>Keel</td>
</tr>
<tr>
<td>G</td>
<td>Centre of gravity</td>
</tr>
<tr>
<td>B</td>
<td>Centre of buoyancy (centre of the underwater displaced volume)</td>
</tr>
<tr>
<td>M</td>
<td>Metacentre</td>
</tr>
<tr>
<td>GM</td>
<td>Metacentric height</td>
</tr>
<tr>
<td>GZ</td>
<td>Righting or Overturning lever</td>
</tr>
</tbody>
</table>

**Initial Stability**

To be adequately stable, the metacentric height (GM) of the loaded vessel, floating upright in still water, is required to be above a minimum value.

- $\text{GM}_{\text{min}} = 0.35$ metres is a recommended minimum guidance value.\(^1\)

The metacentric height can be calculated using the formula:

$$\text{GM} = \frac{KB + BM - KG}{M}$$

(Where the distances between K, B, G, and M are all in metres, KB is the vertical distance from the keel to the centre of buoyancy, BM is the vertical distance from the centre of buoyancy to the metacentre, and KG is the vertical distance from the keel to the centre of gravity.)

The vertical distance between the centre of buoyancy (B) and the metacentre (M), that is $BM = I/V$ (where I is the inertia of the water plane area\(^4\), and V is the volume of displacement.)

For a rectangular water plane area, such as that displaced by a pontoon barge, the ‘roll inertia’ is $I = (l x b^3)/12$, and (for a box shaped barge) the ‘displaced volume’ is $V = (l x b x t)$ (where l is the length, b is the beam, and t is the draught).

**EXAMPLE ONE – HOW TO CALCULATE BM IN PRACTICE**

A box shaped barge 16 metres long, and 6 metres wide floats at a draft of 0.5 metres. Find her BM.

1. $BM = I/V\quad \Rightarrow \quad I = (l x b^3)/12 = (16 x 6^3)/12 = 288$
2. $V = l x b x t\quad \Rightarrow \quad 16 x 6 x 0.5 = 48$

$BM = 288/48 = 6$ metres

\(^1\) The value GM\(_{\text{min}} = 0.35\) metres is from Maritime Rule 40C Appendix 1; 2 (f) (v).

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\(^4\) Inertia of the water plane area is the measure of the resistance offered by the water to movement in one of the six possible directions (roll, pitch, yaw, sway, surge, or heave). The most significant direction – the only movement generally considered in a standard stability analysis – is that of roll (about the longitudinal axis). For roll, the beam of the barge is the main contributor to roll inertia or roll resistance.
For a pontoon shaped barge an approximation for the metacentric height (GM) can be obtained from the rectangular block formula which says:

$$GM = \frac{t}{2} + \frac{b^2}{12t} - h$$

(where \(t\) is the draught, \(b\) is the beam, and \(h\) is the height of the barge, as shown in illustration two).

This formula assumes the barge is a rectangular block with the lightship centre of gravity at deck level. Careful examination of this formula shows the stabilising effect of a beamy barge, referred to above, when considering inertia.

The initial metacentric height (GM) obtained using the rectangular block formula is a fair approximation for a vessel with a block coefficient of about 0.9 and above. The block coefficient is a measure of how close, a particular vessel is to a rectangular block of length x beam x height.

In order to more exactly determine the position of the centre of gravity (G) and the metacentric height (GM) for a particular barge, an inclining experiment needs to be conducted and the results used for a stability analysis. In an inclining experiment weights are moved to the outer edge of the deck of the barge and the heel that results is measured with a pendulum.

An inclining experiment should be undertaken by a Ship Surveyor recognised by Maritime NZ to do so, and the results of the inclining experiment should be analysed by a similarly recognised Naval Architect.

### Static Stability

For stability to be adequate, the righting lever (GZ) resulting from the heeling of a loaded barge is required to be greater than zero (positive) for all angles of heel up to a certain minimum heel angle. 35° is a recommended minimum heel value.

The righting levers arising from different angles of heel are best understood when plotted on a curve. A typical righting lever curve (GZ curve) is shown below in graph one. This particular curve is for a 24m by 8m barge with a loaded displacement of 148 tonnes. It can be seen that the GZ value (measured in metres) is greater than zero for all heel angles up to more than 60°.

GZ curves, such as the one shown, are generated from the stability analysis undertaken by a Naval Architect who will most often use the results from an inclining experiment. Each vessel will have a unique curve depending on displacement, weight distribution and hull shape.

### Dynamic Stability

The area under the GZ curve (and above the horizontal (0) axis), is a product of metres and degrees, and is also an important measure of the stability of a vessel. The larger this area the greater the capacity of the vessel to right itself as it rolls from side to side. This is known as righting energy.

A recommended minimum value for the area under the GZ curve is 5.73 metre x degrees.

The size of this area is determined by the initial GM (which gives the starting slope of the curve), the heel angle at which maximum GZ occurs (which gives the height of the curve) and the range of heel angles for which GZ is positive (which gives the length of the curve).

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2 This value is a simplified summary of Maritime Rules 40C Appendix 1 (2)(f)(iii) and (i), and consistent with Class Society requirements for barging operations.

3 This is a conservative simplification of the requirements of Maritime Rule 2(f)(i).
Combined KG

**ILLUSTRATION THREE – DETERMINING COMBINED KG**

\[
\text{COMBINED KG} = \frac{(\text{KG}_1 \times W_1) + (\text{KG}_2 \times W_2)}{(W_1 + W_2)}
\]

**ILLUSTRATION THREE GLOSSARY**

<table>
<thead>
<tr>
<th>KG1</th>
<th>Vertical distance from keel to G1</th>
</tr>
</thead>
<tbody>
<tr>
<td>KG2</td>
<td>Vertical distance from keel to G2</td>
</tr>
<tr>
<td>W1</td>
<td>Weight 1</td>
</tr>
<tr>
<td>W2</td>
<td>Weight 2</td>
</tr>
</tbody>
</table>

A straightforward check of initial stability involves determining the combined KG value for a barge and its cargo. Illustration three shows a pontoon barge loaded with secured deck cargo. The centre of gravity of the lightship barge is marked as G1 and the centre of gravity of the cargo is marked as G2. The distance from the keel to these positions are the distances KG1 and KG2. The lightship weight of the barge is W1 tonnes, and the cargo weight is W2 tonnes. The combined KG is then obtained using the formula in example two on the facing page.

**EXAMPLE TWO – HOW TO CALCULATE KG IN PRACTICE**

The use of the formula in practice.

\[
\text{KG} = \frac{\text{total moment} ((\text{KG}_1 \times W_1) + (\text{KG}_2 \times W_2))}{\text{total weight} (W_1 + W_2)}
\]

This formula can be tabulated for ease of calculation

<table>
<thead>
<tr>
<th>Barge's weight</th>
<th>Barge's KG</th>
<th>Weight x KG</th>
<th>Barge's moment</th>
</tr>
</thead>
<tbody>
<tr>
<td>Load weight</td>
<td>Load KG</td>
<td>Weight x KG</td>
<td>Load's moment</td>
</tr>
<tr>
<td>Total weight</td>
<td></td>
<td>Total moment</td>
<td></td>
</tr>
</tbody>
</table>

A box shaped barge has a lightship displacement of 85 tonnes and a KG of 1.8 metres. A weight of 65 tonnes with a KG of 3.8 metres is loaded on to the barge deck.

**Calculate the combined KG**

<table>
<thead>
<tr>
<th>Barge's weight</th>
<th>Barge's KG</th>
<th>Weight x KG</th>
<th>Barge's moment</th>
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</tr>
<tr>
<td>Total weight</td>
<td></td>
<td>Total moment</td>
<td></td>
</tr>
</tbody>
</table>

Combined KG = total moment/total weight, which is 400/150 = 2.67 metres.

Answer: combined KG = 2.67 metres

The combined KG and loaded displacement values can then be used for a check on the initial stability of the loaded barge, as described in the next section.
**LIMITING KG CURVES**

A Naval Architect, as part of a stability analysis for a barge, can draw a limiting KG curve. The limiting KG curve is used, in conjunction with the combined KG and loaded displacement to establish whether the loaded condition is safe. The limiting KG curve has safety margins built in. These margins are achieved by using recommended minimum values (such as, initial GM greater than 0.35 metres⁴; vanishing stability (positive GZ) to greater than 35°; and area under the GZ curve not less than 5.73 metre x degrees).

The limiting KG curve such as the one shown opposite enable you to establish how much combined weight (lightship and cargo) can safely be carried, for a known combined KG.

- The area under the curve is a safe load condition.
- The area above the curve is an unsafe load condition.

**EXAMPLE THREE – HOW TO USE LIMITING KG CURVES IN PRACTICE**

Using graph two and the calculated values in example two – ie. combined KG = 2.67 metres, loaded displacement = 150 tonnes – establish if the load condition is safe or unsafe?

It can be seen from graph two that for a loaded displacement of 150 tonnes and combined KG of 2.67 metres the load condition is safe provided the combined KG of the lightship barge and cargo is less than 5 metres.

**Answer:** 2.67 m is less than 5m, therefore the loaded condition is safe.

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⁴ This value is from Maritime Rule 40C Appendix 1 (2)(f)(iv).
OTHER STABILITY CONSIDERATIONS

Crane Outreach

When using cranes and other lifting gear such as A frames that are barge mounted, it must be noted that the weight of the lifted load acts at the point of suspension – not at the base of the crane. The overturning moment on the barge, tending to cause it to capsize, is the product of the weight of the lifted load, and the (horizontal) distance \(d_1\) of the point of suspension \(p\) from the centre of buoyancy \(B\).

\[
\text{CRANE OVERTURNING MOMENT} = d_1 \times W
\]

\[
\text{MAXIMUM UPLIFT FORCE} = d_2 \times W
\]

The greatest uplift or detachment force, acts at the point of attachment (of the crane to the barge) furthest from the point of suspension. This is the force tending to turn the crane over and the moment of this force is the product of the weight of the lifted load, and the (horizontal) distance \(d_2\) of the point of suspension \(p\) from the point of uplift \(u\).

Free surface effect

Fluids such as fuel and water can adversely affect the stability of a moving vessel. As shown in illustration five, the weight of a tank of fluid – acting at the centre of gravity – moves further off the centreline the further the vessel rolls.

Even a shallow covering of water over a large enclosed deck can cause a significant problem. 150 mm of fresh water covering a 24 m by 6 m deck weighs 21.6 tonne, and as the vessel rolls this weight will be transferred outboard to the down side of the roll.

Sloshing is another phenomenon, which can greatly amplify the destabilising effect of a large free surface of fluid. The effect of sloshing is worst if the movement of fluid coincides with the movement of the vessel.

Baffles are used to break up the free surface within a tank and to prevent sloshing. A Naval Architect will be able to offer guidance on the best baffle spacing, and the requirements on baffle strength needed to minimise the adverse effects of free surfaces.
Shifting Cargo
Securing arrangements should be of such design that they are strong enough to prevent any cargo movement during transit.
Maritime Rule part 24B gives prescribed requirements for stowage and securing of all cargoes. It is recommended that Maritime Rule part 24B be read in conjunction with these guidelines.

Loading and Discharge
It is vital that stability is considered during all phases of barge operations, including loading and discharge. The stability conditions during loading and discharge are often quite different from those when fully loaded. Guidance should be sought from a Surveyor or Naval Architect in any cases of doubt.
High loads, moving loads, and off-centreline loading plans all need special consideration. A low initial GM value, a combined KG that is close to or below the required minimum and small righting areas all mean that the loaded barge will have poor recovery characteristics when rolling in a seaway.
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